Measurement and analysis of vibration in the myocardium telescopic motion for novel echo-graphic diagnosis

Hiroshi Kanai¹, Shin-ichi Katsumata¹, Hideyuki Honda² and Yoshiro Koiwa³

¹Graduate School of Engineering, Tohoku University, Aramaki-aza-Aoba 05, Sendai, 980–8579 Japan
²Faculty of Medical Science and Welfare, Tohoku Bunka Gakuen University, Kunimi 6–45–16, Aoba-ku, Sendai, 981–8551 Japan
³Graduate School of Medicine, Tohoku University, Seiryou-machi 1–1, Aoba-ku, Sendai, 980–8574 Japan

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Abstract: We have already developed a novel ultrasonic-based method, namely, the phased tracking method, to measure the rapid velocity in the heart wall by accurately tracking the movement in the heart wall. By applying this method to in vivo experiments, the velocity signal of the heart wall with small amplitude, less than several micrometers on the large motion resulting from a heartbeat, can be successfully detected. There are high frequency components of up to several hundreds Hertz, which have not been previously investigated at all. In this study, after the papillary muscle had been extracted from an isolated rat heart, it was electrically stimulated, and the resultant muscular vibration was directly measured in the frequency range up to 2 kHz using a laser Doppler velocimeter in order to confirm if the high frequency vibrations occur during contraction and relaxation. For the injured myocardium, the power increase in the high frequency components becomes smaller. The experimental results support the hypothesis that the high frequency components are included in the velocity signal measured for the first time in the human interventricular septum by the phase tracking method using ultrasound.

Keywords: Phased tracking method, Myocardium vibration, Myocardium vulnerability

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1. INTRODUCTION

We have already developed a novel ultrasonic-based method, namely, the phased tracking method, to measure the rapid velocity in the heart wall by accurately tracking the movement \( x_i(t) \) of a point \( i \) in the heart wall by the constraint least-squares method applied to both the phase and magnitude of the quadrature-demodulated signals [1]. RF pulses are transmitted from an ultrasonic transducer at a pulse repetition interval \( \Delta T \), and the reflected ultrasonic wave is received by the same transducer and is multiplied by the original RF signal in quadrature-demodulation. By synchronizing the pulse transmission timing and the acquisition timing in A/D conversion rigidly with the original RF signal, the achieved lower limit \( |v_{\min}| \) in the above velocity measurement was 0.1 mm/s, which was confirmed in phantom experiments [2], using the developed method and system [1]. The lower limit depends on the small dispersion in the above synchronization and on the additive noise in the received signal. Since the lower limit \( |v_{\min}| \) is less than 1/2,000 of the upper limit \( |v_{\max}| \) of the measurable velocity, which is free from aliasing, the dynamic range of the velocity measurement is given by \( 20 \log_{10} |v_{\max}|/|v_{\min}| = 73 \text{ dB} \). In other phantom experiments [1], a vibration with small amplitude of 20 \( \mu \text{m} \) generated on the large motion with an amplitude of 7.5 mm and a frequency of 1 Hz, which simulates the heartbeat, was successfully measured in the range from 1 Hz to 1 kHz.

By applying this method and system to in vivo experiments, the velocity signal, \( v(t; x_i) \), of point \( i \) at a depth of \( x_i \) in the heart wall with small amplitude, less than several micrometers on the large motion resulting from a heartbeat, can be successfully detected with reproducibility [1]. By applying frequency analysis to the resultant velocity signal, \( v(t; x_i) \), of the heart wall, the Fourier spectrum of \( v(t; x_i) \) has been obtained for the first time with sufficient reproducibility in the frequency range up to
The developed method has already been realized in a real-time measurement system [3]. Moreover, from the difference of the resultant velocity signals \( v(t; x_i) \) between point \( x_i \) and its succeeding point \( x_{i+1} \) preset along the ultrasonic beam, a minute change in thickness of several tens of micrometers has been detected with a spatial resolution of 0.5 \( \mu \)m [4] as described above.

With the phased tracking method it is possible to accurately detect small amplitude velocity signals of less than a few micrometers in the heart wall [1]. There are high frequency components up to several hundreds Hertz [1] which cannot be recognized in standard B-mode echocardiography, M-mode echocardiography, or in conventional tissue Doppler imaging (TDI). The clinical and physiological meanings and the mechanisms of such high frequency vibrations have not been previously investigated. If the mechanism of the high frequency components can be clarified, it will offer potential for novel quantitative assessment of myocardial viability.

It is known that vibrations along the muscular fibers occur during contraction and relaxation of the skeletal muscle [5–9]. In the literature, there have been many reports of attempts to transcutaneously measure such muscle sounds originating from the muscle vibrations [5–9]. However, the muscle vibrations have been measured only in the frequency range up to 100 Hz.

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2. IN VITRO EXPERIMENTS

A papillary muscle extracted from a rat heart was fixed in a water tank by two tungsten hooks and a force transducer was employed to measure the generated tension \( T(t) \) along the longitudinal axis of the myocardium as shown in Fig. 1. In order to maintain the physiological conditions close to in vivo conditions, Krebs-Henseleit solution was circulated in the water tank by the peristaltic pump and the temperature of the water tank was kept constant at 25 ± 0.2 degrees Celsius.

The myocardium was electrically stimulated through two parallel platinum electrodes by rectangular wave \( e(t) \) with a duration of 1 ms and a repetition frequency of 1 Hz as shown in Fig. 3(a). At the same time, the velocity component \( v(t) \) generated in the direction normal to that of the myocardium was measured at the center of the muscle by a laser Doppler velocimeter (Ono Sokki LV-1300) as shown in Fig. 3(b). The output \( T(t) \) of the force transducer was obtained as shown in Fig. 3(d). These signals were simultaneously A/D converted at a sampling frequency of 50 kHz. They were then transfered to a workstation via a GPIB interface for further frequency analysis.

In order to detect the presence of contaminating noise component \( n(t) \) in the measured velocity \( v(t) \), the velocity component \( v(t) \) at the arm of the tungsten hook was simultaneously measured as shown in Fig. 3(c). By integrating the velocity \( v(t) \) of the myocardium in the workstation, its displacement \( x(t) \) was estimated as shown in Fig. 3(e).

3. IN VITRO EXPERIMENTAL RESULTS

Each signal from Fig. 3(a) to Fig. 3(e) is divided into the respective duration periods and is overlaid in Fig. 2(a) to Fig. 2(e), where the horizontal time axis is expanded.

From Fig. 2(b), the velocity \( v(t) \) of the myocardium included two types of components: one is the low frequency component which is synchronous with the electrically stimulated signal \( e(t) \) in Fig. 2(a), and the other is the high frequency component which seems to be similar to the noise component \( n(t) \) in the time domain of Fig. 2(c).

For detection of the change in power during one duration period in the frequency domain, the velocity signal \( v(t) \) of each duration period in Fig. 3(b) was divided into 39 short-period signals \( \{v(t; i)\} \) \( (i = 1, 2, \ldots, 39) \) by shifting and multiplying the Hanning window with a length of 50 ms from the rising edge \( (T = 0) \) of the electrical stimulation \( e(t) \) of each duration period, where half of the succeeding windows overlapped. Then, the Fourier transform was applied to each signal of \( \{v(t; i)\} \) \( (i = 1, 2, \ldots, 39) \). The resultant power spectra \( \{P(f; i)\} \) up to 2 kHz of the \( i \)th short-period signals \( \{v(t; i)\} \) with the
same delay time from the rising edge were averaged for the 5 duration periods and are plotted in Fig. 4. In Fig. 4, the time origin \((T = 0)\) corresponds to the rising edge of the electrical stimulation \(e(t)\) of each duration period in Fig. 3(a). Each averaged power spectrum was normalized by the averaged power spectrum \(P_0(f)\) at the period 200 ms in length just before the rising edge \((T = 0)\). Thus, the value in Fig. 4 shows the change in the averaged power spectra compared with that just before the contraction.

The same procedure was applied to the noise signal \(n(t)\) in Fig. 3(c) and the change in power spectrum is shown in Fig. 5. There did not seem to be any noteworthy change in power in Fig. 5. In Fig. 4, however, for the contraction period \((0–200\,\text{ms})\) just after the electrical stimulation, there were large increases in power both in the low frequency component less than 25 Hz and in the wide frequency band from 200 Hz to 2 kHz. For the relaxation period \((200–500\,\text{ms})\) as well, there were large increases in power in both of these frequency bands as above. The low frequency component corresponds to the bending displacement of the muscle due to its contraction or the relaxation. For the higher frequency band, the power increased.

For the contraction period of 50 ms around the time \((T_c)\) 75 ms after the rising edge \(T_0\) and for the relaxation period with 50 ms around the time \((T_r)\) 350 ms after \(T_0\), the change in the averaged power spectrum compared with that just before the contraction in Fig. 4 are shown by red lines in Figs. 6(a) and 6(b), respectively. For the noise vibration \(n(t)\) of the hook arm, the results in Fig. 5 are shown by blue lines in these figures.
As indicated by these blue lines, the noise vibration \( n(t) \) did not show a noteworthy increase in power. For the vibration of the myocardium, however, the power increased by about 15–20 dB in the low frequency band less than 30 Hz and in the higher frequency band from 1 kHz to 2 kHz. As indicated by these results, due to the contraction or the relaxation, telescopic vibrations with high frequency components in the frequency band from 1 kHz to 2 kHz, which is other than the displacement, were certainly generated.

Next, in order to compare the characteristics of the above normal myocardium with those of an injured myocardium, for the same papillary muscle after measurement of the signals in Fig. 3, the perfusion with the Krebs-Henseleit solution was completely stopped for 120 seconds. Then, the same measurement and analysis were applied to the injured myocardium.

The results are shown in Figs. 7–11. As for the measurement, the noise component \( n(t) \) in Figs. 7(c) or 8(c) was large. However, this erroneous component was a low frequency component less than 40 Hz and was
cancelled out by the change in the power spectrum component just before the contraction as shown in Fig. 10. Also for the injured myocardium, a wide frequency band component was detected during the contraction and relaxation as shown in Figs. 9, 11(a), and 11(b). For the injured myocardium, however, the power increase was only about 10 dB, which is not so large in comparison with those of the normal myocardium in Figs. 6(a) and 6(b), and the frequency band became lower at the point where the power increased.

4. CONCLUSIONS

In this paper, by electrically stimulating the extracted papillary muscle of rats, the vibration component in the direction normal to the myocardial fiber was measured by a laser Doppler velocimeter. Then, it was analyzed in the frequency domain. From the experimental results, the vibration during contraction and relaxation had a high frequency component from 1 kHz to 2 kHz. For the injured myocardium, however, the power increase in the high frequency component during contraction or relaxation decreased. The experimental results support the fact that the high frequency component is included in the velocity signal measured for the first time for the human interventricular septum (IVS) by the phase tracking method using ultrasound [1]. Thus, the detection of the change in power has potential for diagnosis of the vulnerability of the regional heart muscle.

REFERENCES

Hiroshi Kanai was born in Matsumoto, Japan, on November 29, 1958. He received a B.E. degree from Tohoku University, Sendai, Japan in 1981, and M.E. and the Ph. D. degrees, also from Tohoku University, in 1983 and in 1986, both in Electrical Engineering. From 1986 to 1990 he was with Processing, Tohoku University, as a research associate. From 1990 to 1992 he was a lecturer in the Department of Electrical Engineering, Faculty of Engineering, Tohoku University. From 1992 to 2001 he was an associate professor in the Department of Electrical Engineering, Faculty of Engineering, Tohoku University. Since 2001 he has been a professor in the Department of Electronic Engineering, Graduate School of Engineering, Tohoku University. His present interests are in ultrasonic measurement and digital signal processing for diagnosis of heart diseases and arteriosclerosis.

Shin-ichi Katsumata was born in Sendai, Japan, in 1977. He received a B.E. degree in Electrical Engineering from Tohoku University, Sendai, Japan in 2000. Since 2000, he has been a student of the Department of Electrical and Communication Engineering, Graduate School of Engineering, Tohoku University. His research interests are ultrasonic measurement and digital signal processing for myocardial tissue characterization.

Hideyuki Honda was born in Matsushima, Japan, on June 9, 1953. He received a bachelor of Science Degree from Tohoku University, Sendai, Japan in 1977. He received MD degree and Ph.D. from Tohoku University School of Medicine, in 1985 and in 1992, respectively. From 1985 to 1987, he was a resident fellow at Takeda general hospital, Aizuwakamatsu, Japan. From 1992 to 1995 and 1995 to 1997, he was a Research Associate and Clinical Fellow at Tohoku University School of Medicine. From 1998 to 1999, he was a Research Associate at the University of Illinois at Chicago. Since 1999, he has been an associate professor at Tohoku Bunka Gakuen University. His present interests are basic characteristics of muscles.

Yoshiro Koiwa was born in Sendai, Japan, in 1944. He graduated from Tohoku University, Sendai, Japan, in 1969. He received the M.D. degree from Tohoku University in 1977. He is presently Associate Professor of Internal Medicine of Tohoku University. His main research interest is cardiovascular disease, especially cardiac function and heart failure. Dr. Koiwa is member of American Federation for Clinical Research, the Japanese Circulation Society, and the Japan Society of Medical Electronics and Biological Engineering.