

This is the appendix for the paper “Propagation of Spontaneously Actuated Pulsive Vibration in Human Heart Wall and *In Vivo* Viscoelasticity Estimation” by Hiroshi Kanai published in *IEEE Transactions on Ultrasonics, Ferroelectrics, and Frequency Control*. Vol. 51, No. 11, pp. 1931–1942 (November 2005)

## APPENDIX I

### THEORETICAL EQUATIONS OF A LAMB WAVE PROPAGATING ALONG VISCOELASTIC PLATE IMMERSED IN BLOOD

For the asymmetric Lamb wave in **Fig. 1**, let us assume that the Lamb wave propagates in the positive  $x$ -direction along the plate. The potential  $\phi$  of the primary (longitudinal) wave and the potential in plate,  $\psi$ , of the SV wave are respectively given by

$$\phi = A \sinh(\eta y) \exp(j k_L x) \quad (\text{A.1})$$

$$\psi = B \cosh(\beta y) \exp(j k_L x), \quad (\text{A.2})$$

where  $A$  and  $B$  are amplitude constants,  $j = \sqrt{-1}$ , and  $k_L$  is the wave number. Using the wave numbers  $k_p$  for the primary wave and  $k_s$  for the secondary wave of the plate material, the

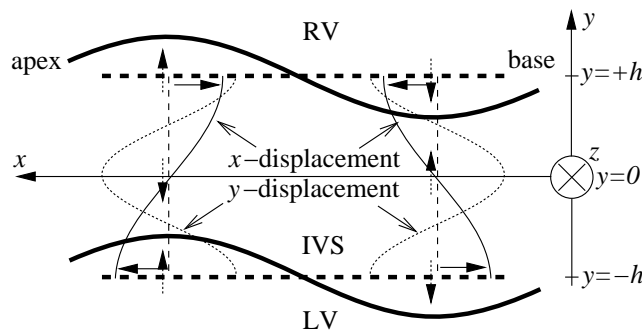


Fig. 1. Lamb wave with asymmetric mode of plate waves in the viscoelastic plate with thickness  $2h$ . The SV-wave component ( $y$ -displacement) and longitudinal component ( $x$ -displacement) are coupled, and the Lamb wave then propagates along the  $x$ -direction. Though a slightly higher order mode is illustrated, the lowest mode is probably dominant in actual vibration in the IVS.

following  $\eta$  and  $\beta$  are defined as

$$\eta = \sqrt{k_L^2 - k_p^2} \text{ [rad/m]} \quad (\text{A.3})$$

$$\beta = \sqrt{k_L^2 - k_s^2} \text{ [rad/m]}. \quad (\text{A.4})$$

Let us assume that the myocardium is isotropic. Using the Lamb wave phase velocity  $c_L$ , the primary wave speed  $c_p$ , the secondary wave speed  $c_s$ , Lamé elastic constants  $\lambda$  and  $\mu$ , and the myocardial density  $\rho_m$ , the wave numbers  $k_L$ ,  $k_p$ , and  $k_s$  are described by

$$k_L = \frac{\omega}{c_L} \text{ [rad/m]} \quad (\text{A.5})$$

$$k_p = \frac{\omega}{c_p} = \omega \sqrt{\frac{\rho_m}{\lambda + 2\mu}} \text{ [rad/m]} \quad (\text{A.6})$$

$$k_s = \frac{\omega}{c_s} = \omega \sqrt{\frac{\rho_m}{\mu}} \text{ [rad/m]}, \quad (\text{A.7})$$

where  $\omega = 2\pi f$  denotes the angular frequency. The displacement  $u_x$  in the  $x$ -direction and  $u_y$  in the  $y$ -direction are thus given by

$$u_x \equiv \frac{\partial \phi}{\partial x} + \frac{\partial \psi}{\partial y} = \{jk_L A \sinh(\eta y) + \beta B \sinh(\beta y)\} \exp(jk_L x) \text{ [m]} \quad (\text{A.8})$$

$$u_y \equiv \frac{\partial \phi}{\partial y} - \frac{\partial \psi}{\partial x} = \{\eta A \cosh(\eta y) - jk_L B \cosh(\beta y)\} \exp(jk_L x) \text{ [m]}. \quad (\text{A.9})$$

From the stress-strain relationship with Lamé constants  $\lambda$  and  $\mu$  for isotropic material, the stress  $\sigma_{yy}$  normal to  $y$ -axis is given by

$$\begin{aligned} \sigma_{yy} &\equiv (\lambda + 2\mu) \frac{\partial u_y}{\partial y} + \lambda \frac{\partial u_x}{\partial x} \text{ [Pa]} \\ &= (\lambda + 2\mu) \left( \frac{\partial^2 \phi}{\partial y^2} - \frac{\partial^2 \psi}{\partial x \partial y} \right) + \lambda \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \psi}{\partial x \partial y} \right) \\ &= (\lambda + 2\mu) \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} \right) - 2\mu \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \psi}{\partial x \partial y} \right) \\ &= \mu \left\{ \kappa^2 \nabla^2 \phi - 2 \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \psi}{\partial x \partial y} \right) \right\}, \end{aligned} \quad (\text{A.10})$$

where

$$\kappa^2 \equiv \frac{\lambda + 2\mu}{\mu} = \left( \frac{c_p}{c_s} \right)^2. \quad (\text{A.11})$$

Using the relation

$$\nabla^2 \phi + k_p^2 \phi = 0, \quad (\text{A.12})$$

the first term of the last equation of Eq. (A.10) is described as follows:

$$\begin{aligned}
\kappa^2 \nabla^2 \phi &= \left( \frac{c_p}{c_s} \right)^2 \nabla^2 \phi \\
&= \left( \frac{k_s}{k_p} \right)^2 \nabla^2 \phi \\
&= -k_s^2 \phi.
\end{aligned} \tag{A.13}$$

Thus, using Eqs. (A.1) and (A.2), the stress  $\sigma_{yy}$  of Eq. (A.10) is given by

$$\begin{aligned}
\sigma_{yy} &= -\mu \left\{ k_s^2 \phi + 2 \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \psi}{\partial x \partial y} \right) \right\} \\
&= -\mu \left\{ (k_s^2 - 2k_L^2) A \sinh(\eta y) + (2jk_L \beta) B \sinh(\beta y) \right\} \exp(jk_L x).
\end{aligned} \tag{A.14}$$

On the other hand, using Eqs. (A.8) and (A.9), the  $y$ -direction shear stress in the plane normal to  $x$ -axis,  $\sigma_{xy}$ , is given by

$$\begin{aligned}
\sigma_{xy} &\equiv 2\mu \times \frac{1}{2} \left( \frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right) \text{ [Pa]} \\
&= \mu \left\{ (2jk_L \eta) A \cosh(\eta y) + (k_L^2 + \beta^2) B \cosh(\beta y) \right\} \exp(jk_L x).
\end{aligned} \tag{A.15}$$

Since the plate is immersed in blood, the acoustic energy of the Lamb wave in the plate leaks into the surrounding blood medium. For the leaky component, the potential  $\phi_b$  of the primary wave in the  $x - y$  plane in blood is given by

$$\phi_b = \begin{cases} -C \exp(-\eta_b y) \exp(jk_b x) & \text{if } y > 0 \\ C \exp(\eta_b y) \exp(jk_b x) & \text{if } y < 0 \end{cases}, \tag{A.16}$$

where  $k_b$  is the wave number in blood and  $C$  is an amplitude constant. The minus sign of the coefficient ( $-C$ ) of the first equation in Eq. (A.16) characterizes the asymmetric mode. Using the velocity  $c_b$  for the primary wave in blood, the following  $\eta_b$  and  $k_b$  are defined by

$$\eta_b = \sqrt{k_L^2 - k_b^2} \text{ [rad/m]} \tag{A.17}$$

$$k_b = \frac{\omega}{c_b} \text{ [rad/m]}. \tag{A.18}$$

For the primary wave in blood leaked from the IVS boundary, the displacement  $u_y$  in the  $y$ -direction, the displacement  $u_x$  in the  $x$ -direction, and stress  $\sigma_{yy}$  normal to the  $y$ -axis are

respectively given by

$$\begin{aligned}
u_y &\equiv \frac{\partial \phi_b}{\partial y} \text{ [m]} \\
&= \begin{cases} \eta_b C \exp(-\eta_b y) \exp(j k_b x) & \text{if } y > 0 \\ \eta_b C \exp(\eta_b y) \exp(j k_b x) & \text{if } y < 0 \end{cases}, \tag{A.19}
\end{aligned}$$

$$\begin{aligned}
u_x &\equiv \frac{\partial \phi_b}{\partial x} \text{ [m]} \\
&= \begin{cases} -j k_b C \exp(-\eta_b y) \exp(j k_b x) & \text{if } y > 0 \\ j k_b C \exp(\eta_b y) \exp(j k_b x) & \text{if } y < 0 \end{cases}, \tag{A.20}
\end{aligned}$$

$$\begin{aligned}
\sigma_{yy} &\equiv \lambda_b \left( \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} \right) \text{ [Pa]} \\
&= \lambda_b \left( \frac{\partial^2 \phi_b}{\partial x^2} + \frac{\partial^2 \phi_b}{\partial y^2} \right) \\
&= \lambda_b \nabla^2 \phi_b \\
&= -\lambda_b k_b^2 \phi_b \\
&= -\rho_b \omega^2 \phi_b \\
&= \begin{cases} \rho_b \omega^2 C \exp(-\eta_b y) \exp(j k_b x) & \text{if } y > 0 \\ -\rho_b \omega^2 C \exp(\eta_b y) \exp(j k_b x) & \text{if } y < 0 \end{cases}, \tag{A.21}
\end{aligned}$$

where  $\lambda_b$  is the Lamé constant in blood,  $\rho_b$  is the blood density ( $= 1.1 \times 10^3 \text{ kg/m}^3$ ),  $\partial u_x / \partial x = -k_b^2 \phi_b$ , and  $\partial u_y / \partial y = \eta_b^2 \phi_b$ , and the following relation is used.

$$k_b = \omega \sqrt{\frac{\rho_b}{\lambda_b}} \tag{A.22}$$

By applying the vanishing shear stress ( $\sigma_{xy}$  of Eq. (A.15)) condition at the myocardium-blood interfaces ( $y = \pm h$ ), continuity of the normal stress ( $\sigma_{yy}$  of Eqs. (A.14) and (A.21)), and the continuity of the displacement ( $u_y$  of Eqs. (A.9) and (A.19)) across the two interfaces at  $y = \pm h$ , the following three equations are obtained.

$$\begin{aligned}
\sigma_{xy} \Big|_{y=\pm h} &= \mu \left\{ (2j k_L \eta) A \cosh(\eta h) + (k_L^2 + \beta^2) B \cosh(\beta h) \right\} \exp(j k_L x) \\
&= \mu \left\{ (2j k_L \eta) A \cosh(\eta h) + (2k_L^2 - k_s^2) B \cosh(\beta h) \right\} \exp(j k_L x) \\
&= 0 \tag{A.23}
\end{aligned}$$

$$\begin{aligned}
\sigma_{yy} \Big|_{y=\pm h} &= -\mu \left\{ \pm(k_s^2 - 2k_L^2) A \sinh(\eta h) \pm (2j k_L \beta) B \sinh(\beta h) \right\} \exp(j k_L x) \\
&= \pm \rho_b \omega^2 C \exp(-\eta_b h) \exp(j k_L x) \tag{A.24}
\end{aligned}$$

$$\begin{aligned}
u_y \Big|_{y=\pm h} &= \left\{ \eta A \cosh(\eta h) - j k_L B \cosh(\beta h) \right\} \exp(j k_L x) \\
&= \eta_b C \exp(-\eta_b h) \exp(j k_L x).
\end{aligned} \tag{A.25}$$

Since these three equations hold for all  $x$ , the term  $\exp(j k_L x)$  in both sides can be eliminated and the remaining equations are rewritten in the matrix form

$$\begin{pmatrix} 2j k_L \eta \cosh(\eta h) & (2k_L^2 - k_s^2) \cosh(\beta h) & 0 \\ (2k_L^2 - k_s^2) \sinh(\eta h) & -2j k_L \beta \sinh(\beta h) & -\frac{\rho_b k_s^2}{\rho_m} \exp(-\eta_b h) \\ \eta \cosh(\eta h) & -j k_L \cosh(\beta h) & -\eta_b \exp(-\eta_b h) \end{pmatrix} \begin{pmatrix} A \\ B \\ C \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}, \tag{A.26}$$

where the myocardial density  $\rho_m$  is introduced based on the relationship of  $k_s = \omega \sqrt{\rho_m/\mu}$  of Eq. (A.7). For nontrivial solution of  $A$ ,  $B$ , and  $C$ , the following determinant  $\Delta$  of the  $3 \times 3$  matrix should be zero.

$$\begin{aligned}
\Delta &= -\eta_b \exp(-\eta_b h) \left\{ 4k_L^2 \eta \beta \cosh(\eta h) \sinh(\beta h) - (2k_L^2 - k_s^2)^2 \sinh(\eta h) \cosh(\beta h) \right\} \\
&\quad + \frac{\rho_b k_s^2}{\rho_m} \exp(-\eta_b h) \left\{ 2k_L^2 \eta - (2k_L^2 - k_s^2) \eta \right\} \cosh(\eta h) \cosh(\beta h) \\
&= 0.
\end{aligned} \tag{A.27}$$

Therefore, the following function, termed  $f(k_L, k_p, k_s)$ , should zero.

$$\begin{aligned}
f(k_L, k_p, k_s) &\equiv 4k_L^2 \eta \beta \cosh(\eta h) \sinh(\beta h) - (2k_L^2 - k_s^2)^2 \sinh(\eta h) \cosh(\beta h) \\
&\quad - \frac{\rho_b \eta k_s^4}{\rho_m \eta_b} \cosh(\eta h) \cosh(\beta h) = 0.
\end{aligned} \tag{A.28}$$

This function is employed in Eq. (2) of Section III-B.